

TECHNICAL NOTE

Date: 5th August 2021

File Ref: PZ/VL/P21-2319/01TN – Theberton House

Subject: Theberton House Estate – Deadline 6 Noise

1.0 DEADLINE 6 SUBMISSION

- 1.1 Create Consulting Engineers Ltd (Create) have been appointed by our Client (LJ & EL Dowley) located close to the village of Theberton to provide a written submission for “Deadline 6” in line with the Planning Inspectorate timescale.
- 1.2 The Theberton House Estate lies towards the West of the existing Sizewell Power Station and as part of the access arrangements to serve the proposed scheme, a new five-arm roundabout is proposed on the B1122 Abbey Road to the East of Leiston Abbey.
- 1.3 The purpose of this submission is to provide further technical information to inform PINs on the shortfalls highlighted at Deadline 5 relating to noise matters only.
- 1.4 As noted at DL5 following the ISH2/3 there are several significant points which the Applicant has also failed to adequately address. These points have yet to be reported on and therefore Create reserve the right to comment further on these points at DL7.
- 1.5 We would urge the Applicant to engage directly with our Client given the conflicting information we are receiving from their Agent and the time taken to receive the requested information, giving little or no time to respond. The Applicant’s lack of engagement since 2019 has been lamentably minimal.

2.0 THEBERTON HOUSE – NOISE

2.1 At ISH2, Mr Humphreys highlighted that there was to be a separate ISH on Noise. Create are pleased to see this has now been added to the ISHs on Wednesday 25th August 2021.

2.2 In summary, at DL5 Create stated the following.

Deadline 5 – Summary of Submission - Noise

2.3 The ES details a preliminary assessment of construction noise, undertaken in accordance with Method 1 of BS5228-1:2009+A1:2014. The aforementioned standard details two acceptable methodologies for assessment of construction noise. Method 1: the “ABC Method”, and Method 2: the “2-5 dB(A) Change” method. Selecting an appropriate method is discretionary and whilst both are acceptable in broad terms, a distinction should be made based on the situational context at this rural location.

2.4 The threshold noise levels have also been stated incorrectly. Table 3.12 of LA111 (DMRB) suggests that the SOAEL is determined by Section E3.2 and Table E.1 of BS 5228-1. This would result in noise thresholds being set at 65 dB $L_{Aeq,T}$ for day times. It appears however that the thresholds have been set using Table E.2 of BS 5228-1 which is used for eligibility for noise insulation, or for determining the noise insulation trigger level.

2.5 The Assessment provided by the Applicant is considered preliminary only. Assessments of the anticipated works were not based on any contractor method statements, plant schedules or construction phase staging. The construction noise calculations (and in turn, the resultant effects), therefore, have been based on ‘professional judgement’ and assumptions on behalf of the acoustic consultants. Whereas this would be considered appropriate to assess a site’s viability for development, it would not be considered representative of the actual resultant noise levels during phased works and thus on our Client’s home and land interests.

2.6 To date, there has been no dedicated construction noise assessments conducted for the receptor sites. For example, the ‘Enabling Works’ Table (Appendix 4A1, Volume 6.5), has assessed the construction noise for this phase against the sound levels produced by a single excavator alone. It is not clear where the information for calculating the resultant impact at the Fordley Road *et al* residences originated; however, this assumptive approach would not be considered robust or exhaustive to assess any resultant impact in practice.

2.7 The Mitigation Route Map (8.12) details various measures of mitigation for specific works phases in broad terms, stipulating adherence to BPM ‘Best Practicable Means’ and the CoCP ‘Code of Construction Practice’. These mitigative strategies have been based on the assumed construction activities (as discussed above) and have not been directly quantified at the receptor locations to judge their effectiveness.

- 2.8 The reported ambient levels in section 4.4.5 of the ES states the 'Typical Measured Level – Day' at SLR 9 (Representative of Theberton House) was 43-44 dB $L_{Aeq,T}$. Using the ABC method, a negligible impact would be a resultant sound level ≤ 65 dB(A) $L_{Aeq,T}$, which could be up to ≈ 21 dB greater than the measured ambient level. Table 4.15 estimates the work phase noise at the receptor locations to be:
- Preparatory Works: 31-55 dB $L_{Aeq,T}$
 - Main Construction Phase: 58-63 dB $L_{Aeq,T}$
- 2.9 The upper limit of the preparatory works has been calculated to be above the measured residual ambient by 11 dB, which has been deemed to be of a negligible impact. The upper limit of the main construction phase has been predicted to be 19 dB above the residual ambient, for which a moderate adverse significance has been determined (as detailed in the Applicants Table 4.16). Both exceedances would be considered excessive.
- 2.10 Create consider an appropriate assessment method is to use the 2-5 dB(A) change method. Noise levels generated by site activities are deemed to be potentially significant if the total noise (pre-construction ambient plus site noise) exceeds the pre-construction ambient noise by 5 dB or more, subject to lower cut-off values of 65 dB, 55 dB and 45 dB $L_{Aeq,T}$ from site noise alone, for the daytime, evening and night-time periods, respectively; and a duration of one month or more, unless works of a shorter duration are likely to result in a significant effect.
- 2.11 Section 4.3.26 states: *"For noise sensitive receptors where the magnitude of change in the short term is minor, moderate or major at noise sensitive buildings, local circumstances must also be considered to determine the final significance, as required by LA111."* As the new road would be used by most/all of the construction traffic for the next 10+ yrs, this would be indicative of a significant effect, in addition to the operational phase going forward beyond this point and should be assessed and mitigated.
- 2.12 Further dialogue with the Applicant's Agent has confirmed that 30 minute noise measurements took place during 2019. Whilst we accept there is no set measurement duration, typically the minimum measurement duration would be one hour measurement between the hours of 10:00h and 17:00h for daytime hours and the minimum duration for the night time would be 15 minutes. Relying on only a small handful of short measurements automatically increases the uncertainty and reduces the reliability of the noise measurements. Given the importance of these levels when producing an ES, the longer the measurement the better and more reliable the results. In essence, the shorter measurement only captures the noise levels at that particular time.
- 2.13 The author also noted that there was a train for one minute of those 30 minutes, occasional aircraft (which in a rural location can be heard for a long time) and the rustle of vegetation. By virtue, the $L_{Aeq,T}$ is a logarithmic average of the sound levels over the period of time (T) and as these are energy calculations are weighted towards the higher sound levels, as opposed to

the arithmetical averaging method. The fact that there was vegetation rustling, would suggest that the breeze was slightly more than “moderate” which again can artificially increase these sound levels, thus we believe the noise monitoring benchmarking is inadequate.

- 2.14 To accurately gauge the ambient sound level for a day, industry guidance recommends to establish the typical sound level, which would be the most commonly occurring hour long measurement between the hours of 07:00h to 23:00h. That is simply not possible when you are working with one or two 30 minute readings.

3.0 NEW TECHNICAL INFORMATION – NOISE

3.1 Create, attach, at Appendix A the following information;

- New detailed noise monitoring records;
- New detailed noise assessment of background noise levels;
- New predicted noise levels during construction
- New predicted noise levels post construction

3.2 The results are clear and confirm that the baseline sound levels used for the previous noise assessment were approximately 6 – 7 dB above the most commonly occurring day time ambient sound level.

3.3 We are seeking a full and conclusive construction noise and vibration assessment be completed for the Sizewell Link Road and the Main Development Site once the method statements have been finalized and suitable noise mitigation be implemented to reduce the impact of the construction noise.

3.4 The use of earth bunds are limited at best and would be required to be positioned either close to the receptor or the noise source to maximise their efficacy. The SoundPlan model has shown that at this location, the proposed noise mitigation would only achieve approximately 2 dB reduction in sound levels. Additional near field screening would be required around some of the noisier items of plant.

3.5 The use of Best Practicable Means (BPM) must be adhered to, which should include the use of mufflers or silencers, nearfield screening, considerate placement of noisy plant, starting the ignitions in a synchronized manner and not leaving the engines running when not in use. These are examples only and by no means are an exhaustive list.

4.0 CONCLUSIONS

- 4.1 Create have reviewed the Applicant's position. Whilst this DL6 Rep focuses specifically on noise, it has been shown that several important areas have been missed, or remain unanswered, which could misrepresent the final impact outcome.
- 4.2 Our Client and Create have raised significant, legitimate concerns with respect to the SLR and it is requested that the Applicant responds accordingly which in turn could potentially lead to the introduction of mitigation measures and/or redesigned components of the overall scheme currently being put forward.

Note By: Paul Zanna - Technical Director



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**SIZEWELL CLINK ROAD: THEBERTON HOUSE ESTATE
Construction And Operational Noise Assessment**

**SIZEWELL C LINK ROAD:
THEBERTON HOUSE ESTATE
Construction And Operational Noise
Assessment**

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Reference: BD/VL/P21-2319/02

Date: August 2021

**SIZEWELL C LINK ROAD: THEBERTON HOUSE ESTATE
Construction And Operational Noise Assessment**

SIZEWELL C LINK ROAD: THEBERTON HOUSE ESTATE CONSTRUCTION AND OPERATIONAL NOISE ASSESSMENT

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Registration of Amendments

Revision and Date	Amendment Details	Revision Prepared By	Revision Approved By

1.0 EXECUTIVE SUMMARY

About the Authors

- 1.1 This report has been compiled by, Ben Dixon , BA(Hons), PGDip IoA, AMIOA and Mat Tuora , BSc(Hons), PGDip IoA, MIOA, and checked by Jody Blacklock, BEng(Hons), PGDip IoA, MIOA, MCIBSE.

Jody Blacklock - Technical Director

- 1.2 Jody is a Chartered Engineer and Acoustic Consultant with over 20 years' experience. He is the Technical Director for the acoustics team across the business and is responsible for managing the Chelmsford office.
- 1.3 Jody has experience as an Expert Witness and has been involved in a number of multidisciplinary projects since joining the Create in 2017. He has an extensive knowledge of acoustics and is adept at noise modelling and the completion of noise impact assessments. Recently Jody was voted by other acoustic professionals into the role of the Eastern Branch Secretary for the Institute of Acoustics.
- 1.4 Prior to joining Create Jody worked as a Senior Acoustic Consultant for 10 years at dB Attenuation Ltd.

Ben Dixon AMIOA – Principle Acoustic Consultant

- 1.5 Ben is a Principal Acoustics Consultant and Associate Member of the Institute of Acoustics. Prior to joining the acoustic industry in 2013, Ben worked as a Dryliner where he gained a wealth of practical knowledge in the construction environment. After working on site, Ben returned to university to complete his studies. The findings of his dissertation were presented at the Institute of Acoustics, and subsequently published in the Institute's monthly publication.
- 1.6 Ben joined Create in 2018. Prior to joining Create, he worked for BL Acoustics and Stroma Technology where he developed an extensive knowledge of architectural acoustics.

Mat Tuora - Senior Acoustic Consultant

- 1.7 Mat is a Senior Acoustics Consultant with over 7 years of experience, who recently joined Create. Prior to joining our team, Mat held several roles at Adrian James Acoustics, where he gained experience working on a wide range of projects for a variety of high profile local and national clients.

- 1.8 Over the first few years in the industry Mat was responsible for reverberation assessments and pre-completion testing. Since then, Mat was involved in far larger and complex schemes, becoming adept at carrying out detailed environmental assessments, acoustic modelling, and multistage building acoustic design. Mat has also supported several expert witnesses by carrying out calculations and drafting reports. He is a proactive Member of the Institute of Acoustics and recently spent time presenting on work undertaken in call centers for the Institute of Acoustics 2020 Conference.

Report Context and Executive Summary

- 1.9 The following assessment has examined the project specific documentation submitted by EDF Energy (specifically the Environmental Statement and its associated technical documentation) to evaluate the potentially negative acoustical effects of noise arising from the construction and operation of the Sizewell C link road, on the Theberton House Estate residence. This report also includes the evaluation of the sounds arising from the Main Development Site from the construction at the Theberton House Estate residence. The activities within the Main Development site that pose the greatest risk to the NSR are the Phase 1 activities and the proposed 5-arm roundabout.
- 1.10 The EDF documentation contained the methodologies and works phasing that informed EDF's initial assessments. The documentation also contains predictions of changes in noise levels arising from anticipated future traffic flows associated with the operation of the road.
- 1.11 The predicted results of these documents have been compared to the results of a baseline noise survey undertaken by Create Consulting Engineers Ltd (Create), as well as to local, national and international guidance.
- 1.12 This report has used the EDF documentation and industry standard empirical data (later described, herein) to predict and determine noise levels as they may be experienced at the Theberton House Estate.
- 1.13 The results from a noise survey carried out by Create have been used in support of this assessment, to compare against those presented within the EDF ES. The ES stated levels were found to be $\approx 6 - 7$ dB greater than those measured by Create, although not directly comparable in terms of location.
- 1.14 Although indicative, the construction noise calculations provided by EDF should not be considered as robust or exhaustive, as they are suitable for outline scoping only. Primary measures of mitigation have been determined to be necessary within the ES, however further assessment would be warranted to determine whether secondary mitigation would be required.

- 1.15 The transport noise assessment within the ES was found to be within acceptable tolerances, and the stated significance/magnitude of effects within the ES apply.
- 1.16 The ES does not consider loss of external amenity, for which it has been assumed would be potentially significant, depending on the context. This should be considered when defining suitable measures of mitigation.

2.0 INTRODUCTION

- 2.1 Create Consulting Engineers Ltd (Create) have been commissioned by LJ and EL Dowley to undertake a detailed review of the supporting noise and vibration measurements as well as undertaking individual Construction and Operational Noise Assessments to assess proposed works processes for the construction and future use of the Sizewell C link road.
- 2.2 This baseline assessment has defined the anticipated working noise limits for the construction, and quantified the anticipated future noise levels arising from traffic increases at the property boundary of Theberton House Estate. The purpose of this was to ensure the amenity of the residents will be protected.

Site Context

- 2.3 The site is approximately 101 ha and comprises of predominately agricultural land (which accounts for approximately 92.8 ha of the site) as well as highway land and hardstanding. Approximately 76.5 ha of the agricultural land would be required permanently for the proposed development and approximately 16.3 ha would be required temporarily to facilitate the construction.
- 2.4 The route of the Sizewell link road would bypass a section of the B1122 with a new 6.8km long single carriageway road to the south-west. The proposed road would be 7.3 metres (m) wide, with additional 1m hardstrips and 2.5m wide verges. Along the route of the Sizewell link road, there would be swales approximately 3.5m wide for highway drainage.
- 2.5 The road will have a designed speed limit of 60mph, and starts at the A12 south of Yoxford, bypasses Middleton Moor and Theberton before joining the B1122 to the west of the Sizewell C main development site. This proposed development would be retained following completion of the Sizewell C main development site as a lasting legacy of the Sizewell C Project.
- 2.6 It has also been stated that once operational, it would be open to the public and will be used by SZC Co. during the construction phase of the Sizewell C main development site, to transport construction workers arriving by car, buses from both the northern and the southern park and ride sites, and goods vehicles (both light and heavy) delivering freight to the Sizewell C main development site.
- 2.7 The EDF Sizewell Environmental Statement (EDF ES) has split the proposed development into six main areas as follows:
- Area 1 – from the A12 to Footpath E-344/013/0 and E584/016/A (land west of the East Suffolk line);
 - Area 2 – from land west of the East Suffolk line to Littlemoor Road;

- Area 3 – from Littlemore Road to east of Garden House Farm (including the link to B1122 west of Middleton Moor);
- Area 4 – from east of Garden House Farm to land to the west of Theberton;
- Area 5 – from land to the west of Theberton to the south of Theberton; and
- Area 6 – from the south of Theberton to the B1122 adjacent to Brown's Plantation.

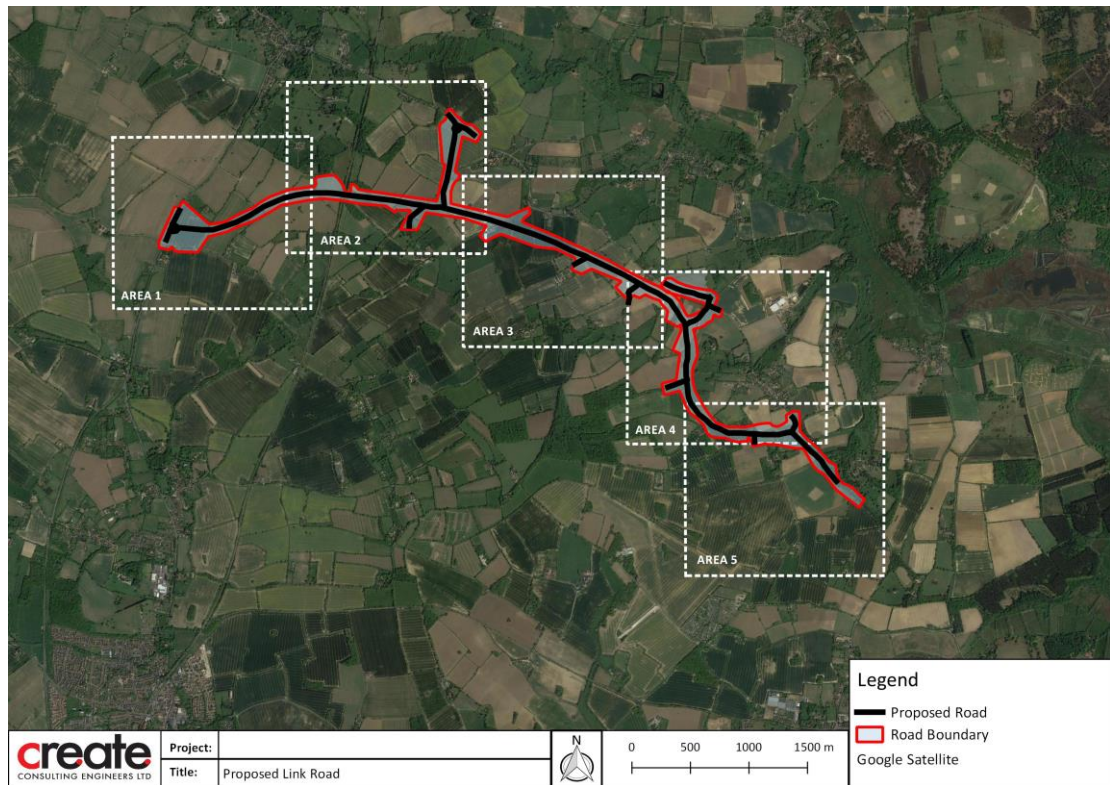


Figure 2.1: Sizewell Link Road. *N.B. Area 6 Location not Illustrated in the ES Chapter*

- 2.8 The Theberton House Estate has been identified in 6.7 Volume 6 Sizewell Link Road Chapter 4 Noise and Vibration Figures 4.1 – 4.2 as Noise Receptor 18 and falls within the boundary of Area 5, which has been shown in greater detail in the following figure:

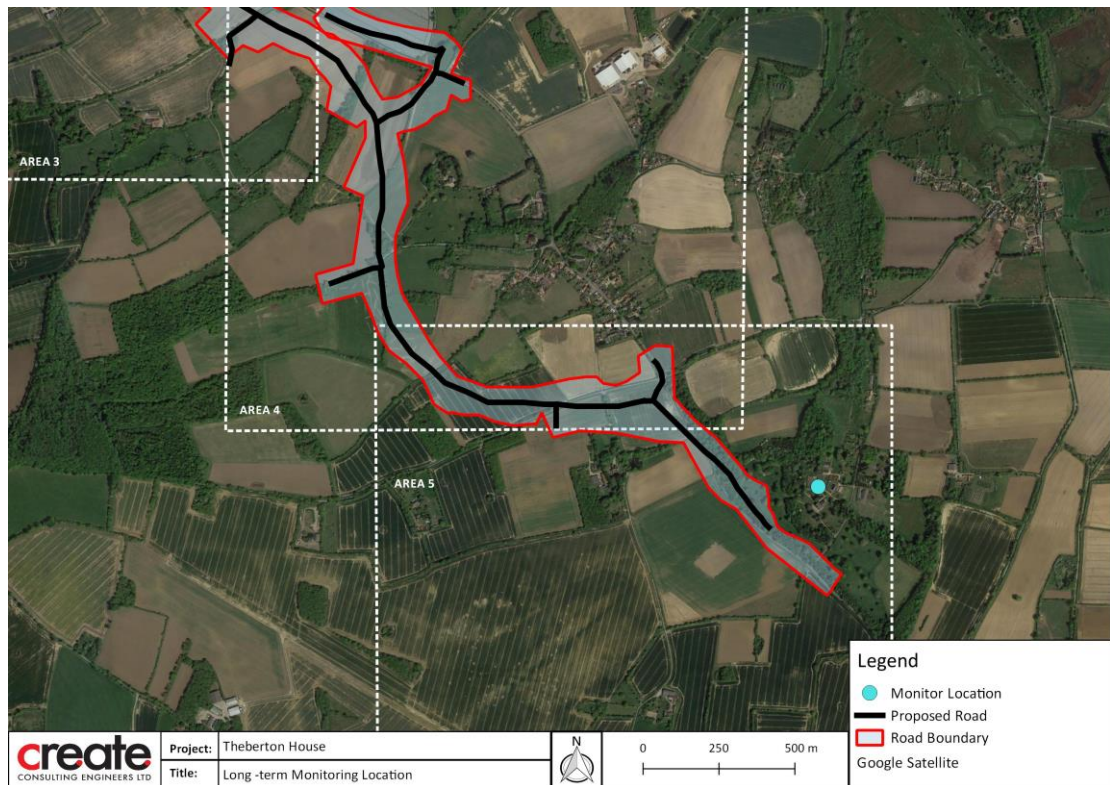


Figure 2.2: Location of Theberton House Estate in Area 5

2.9 Key features of the proposed development in Area 5 include:

- A new ghost island junction would be formed with an extension of the B1125 and a new junction would be formed with a reconfiguration of the existing B1122 (Leiston Road). This includes a provision of a new link road between the route of the proposed Sizewell link road and Leiston Road (the 'B1125 link');
- At the northern end of the B1125 link, Footpath E-396/015/0 would be realigned to meet the new junction between the Sizewell link road and the B1122;
- A portal culvert, 5.4m wide and 1.2m above bank level, would be provided where the route of the proposed Sizewell link road crosses an unnamed watercourse, approximately 200m north west of the existing Pretty Road;
- A new priority junction on the west side of the Sizewell link road at Pretty Road would be provided where the road would be located in a cutting up to 2m deep;
- A new overbridge, single span, up to 44m long would be provided which would carry non-motorised users only (pedestrians, cyclists, equestrians) over the Sizewell link road and connect to Pretty Road on either side. The bridge would be 4m above existing ground level and the Sizewell link road would be in a 5m cutting. The height of the bridge from Sizewell link road level to the top of parapet would be approximately 9m;
- A diversion of Footpath E-396/015/0 where it would be intersected by the Sizewell link road. On the north side of the Sizewell link road, the footpath would be diverted south for approximately 75m to join Footpath E-515/005/0, which would direct users

to Pretty Road. Users would then be able to cross the Sizewell link road via the proposed Pretty Road overbridge. On the south side of the Sizewell link road, users would be diverted south, around the new priority junction and be able to cross the Sizewell link road via the proposed Pretty Road overbridge;

- A diversion of Footpaths E-515/003/0 and E-515/004/0. Users of Footpath E-515/003/0 heading north would be directed north-west to cross the Sizewell link road via the proposed Pretty Road overbridge. Users heading south from Pretty Road would be directed east to join Footpath E-515/004/0. Footpath E-515/004/0 would be diverted east, to cross the proposed road at grade, approximately 50m east of its existing location; and
- A portal culvert, 5.4m wide and 1.2m above bank level, would be provided where the route of the proposed Sizewell link road crosses the Theberton Watercourse, approximately 450m east of the existing Pretty Road.

2.10 There has also been the proposal for a new 5-arm roundabout located approximately 700mtrs south-east of Theberton House Estate. As this section is classed as part of the main development site, it was not assessed as part of the SLR construction.

2.11 Review of the submitted documentation indicate that this was not assessed from a noise perspective as part of the main development, and as such has not had the resultant or cumulative effects quantified at the Theberton House Estate NSR. Given the distance to the site, this would warrant assessment, for which the client have commissioned Create to undertake.



Figure 2.3: Proposed Roundabout

- 2.12 In addition to the points above, there also remains the potential for adverse impact at the NSR from sounds arising within the establishment of the Temporary Construction Area (TCA) within the Main Development Site.

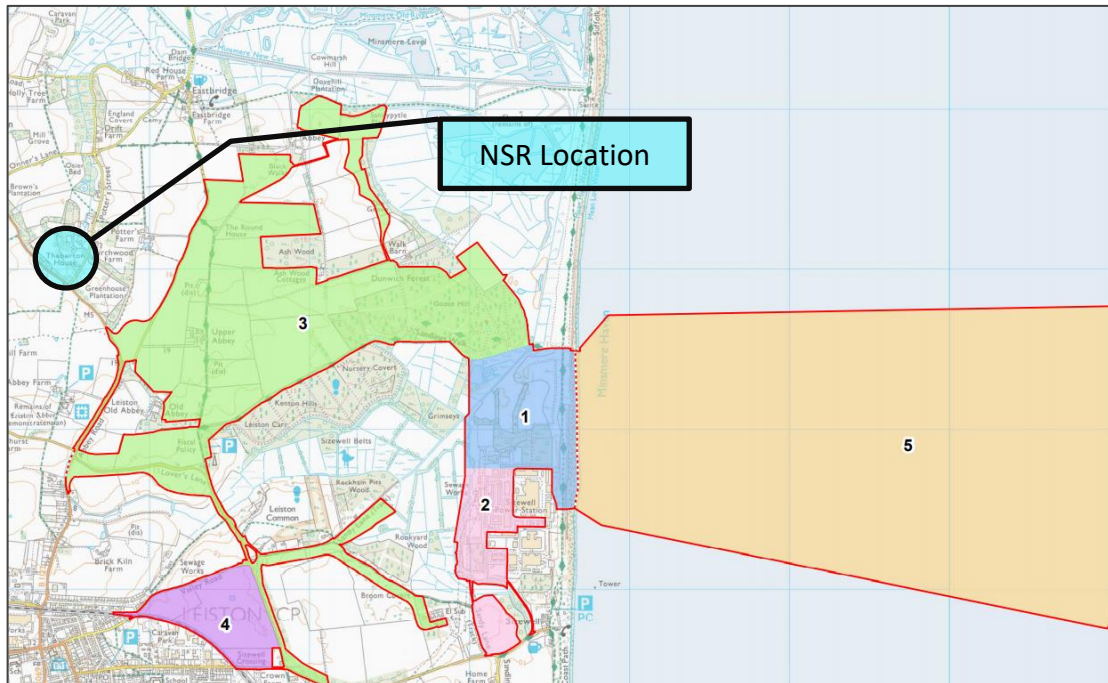


Figure 2.4: TCA (Area 3) Excerpt from Book 6, Chapter 2, Volume 1, Figure 1.1

- 2.13 The Theberton House Estate residence is approximately 600mtrs west of Area 3 'Temporary Construction area' (Figure 5.2, Book 6, 1 Non-Technical Summary) and review of the supporting documentation (Book 6.3, Chapter 11, Construction Noise and Vibration Appendix 11B) states that the construction will comprise of 5 distinct phases (with anticipated, inevitable overlap):

- Phase 1: Site establishment and preparation for earthworks (Years 1 – 2);
- Phase 2: Main earthworks (Years 1 – 4);
- Phase 3: Main civils (Years 3 – 9);
- Phase 4: Mechanical and Engineering (M&E) fit out, instrumentation and commissioning (Years 4 – 11); and
- Phase 5: Removal of temporary facilities and restoration of the land (Years 10 – 12).

- 2.14 Phase 1 will see the site established for the commencement of mineral extraction from the 'borrow pit' sites, which along with other requirements, will be used to supply aggregate to the Main Development Site in Phase 2.

3.0 ASSESSMENT METHODOLOGY AND CRITERIA

- 3.1 This section has outlined the assessment methodology and the significance criteria that have been used to assess the significance of risk associated with the proposed development.

Data Sources

- 3.2 The key data sources reviewed as part of this study have been listed in Table 3.2 below.

Data Source	Reference
British Standards Institute (BSI)	BSI (2009). BS 5228-1:2009+A1:2014 Code of practice for noise and vibration control on construction and open sites: Noise & Vibration
	BSI (2014). BS 8233:2014 Guidance on sound insulation and noise reduction for buildings
	BS6472-1:2008 Guide to Evaluation of Human Exposure to Vibration in Buildings
	BS7385-2:1993 Evaluation and Measurement for Vibration in Buildings
Design Manual for Roads and Bridges	LA 111 – Noise and Vibration

Table 3.1: Key Information Sources

- 3.3 This assessment has considered the existing ambient noise levels and the likely significant effects on existing and proposed human receptors within the site and surrounding area in terms of:

- existing baseline conditions;
- noise impacts expected during construction; and
- Vibratory impacts expected during construction.

BS5228-1 - Noise

- 3.4 Guidance relating to the prediction and assessment of the construction phase noise effects has been taken from BS 5228-1: 2009+A1:2014 'Code of practice for noise and vibration control on construction and open sites' Part 1: 'Noise'¹ which provides recommendations for basic methods of noise control relating to construction and open sites where work activities/operations generate significant noise levels.
- 3.5 Amongst other things, the annexes to BS 5228 provide information on the following:

¹ British Standards Institute. (2009). BS 5228-1:2009+A1:2014 Code of practice for noise and vibration control on construction and open sites. Part 1: Noise. BSI, London.

- relevant legislation (Annex A);
- typical noise sources and advice on mitigating them (Annex B);
- sound level data for use in the prediction methods described in the standard (Annexes C and D);
- assessing the significance of noise effects (Annex E);
- estimating noise levels (Annex F); and
- implementing noise monitoring (Annex G).

BS5228-2 – Vibration

- 3.6 In a similar vein to the British Standard for noise, this refers to vibration levels and the requirement for consideration of the effect of vibration on persons living and working in the vicinity of construction sites.
- 3.7 It provides guidance for the protection from vibrational exposure for persons working on site, as well as neighbourhood nuisance from vibration.
- 3.8 This document also contains many useful annexes at the rear of the Standard, including the following areas:
- Relevant legislation – Annex A;
 - Significance of Vibration Effects. This includes guidance on the human response to vibration, as well as threshold values for effects, structural damage and cosmetic damage – Annex B;
 - Measured levels for piling – Annex C and D;
 - Prediction of Vibration Levels – Annex E;
 - Description of Piling – Annex F.

Design Manual for Roads and Bridges (DMRB LA 111)

- 3.9 This document sets out the requirements for assessing and reporting the effects of highways noise and vibration from construction, operation and maintenance projects.
- 3.10 The requirements in this document shall be applied to the assessment, reporting and management of environmental effects, specifically changes in noise and vibration emissions, from the delivery of projects.

BS6472-1:2008 Guide to Evaluation of Human Exposure to Vibration in Buildings

- 3.11 Structural vibration can often be detected within buildings by the occupants, potentially affecting their quality of life. This document provides guidance on predicting a human's response to vibration in buildings over the frequency range 0.5Hz to 80Hz.

- 3.12 BS6472 describes how to determine the vibration dose value (VDV) from frequency weighted vibration measurements.

BS7385-2:1993 Evaluation and Measurement for Vibration in Buildings

- 3.13 This document provides guidance on the assessment of the possibility of vibration-induced damage in buildings due to a variety of sources, including blasting, piling, machinery and road/rail.
- 3.14 It provides guidance on the correct measurement of Peak Particle Velocity (PPV) whilst also providing within Table 1, the transient vibration guide values for cosmetic damage.

4.0 ACOUSTIC SURVEY PROCEDURE

- 4.1 To ascertain pre-existing sound levels in the immediate area, environmental noise monitoring was undertaken at the Theberton House Estate Noise Sensitive receptors (NSR) to the proposed site between Monday 26th July and Wednesday 4th August 2021.
- 4.2 The microphones were secured to extendable fixtures and the meters were set to capture $L_{Aeq,T}$, $L_{AMAX,F}$ and $L_{feq,T}$ (from 6.3 Hz to 20 kHz) in one second logs and stored the data in 1hr file durations. The Norsonic software NorReview was used to evaluate, post process and calculate the $L_{A90,T}$ and $L_{A10,T}$ values.
- 4.3 The long-term monitor location was selected to measure the residual sound levels at the NSR, and the results of which have been deemed as representative. The location selected (herein referred to as MP1) has been shown in the following figure below with more details included in Appendix B:



Figure 4.1: Measurement Location

- 4.4 A weather station was also deployed during the monitor installation period and set to run continuously throughout. The weather station recorded intermittent periods of inclement weather which have been omitted from calculations and have not been presented in the body of this report. Full Results (including the excluded time periods) can be found in the appendix of this document.

The omitted weather included any periods of substantial rainfall and where wind speeds exceeded >5m/s.

Equipment List

4.5 The sound level meters and acoustic calibrator detailed below were Class 1 standard in accordance with the British Standards 60942 and 61672. They were all within the laboratory calibration time-frame of 2yrs during the period of measurement.

4.6 The equipment detailed below was used for all measurements referenced in this report.

Equipment	Make	Model	Serial Number
Sound Level Meters	Norsonic	Nor 140	1406178
Acoustic Calibrator	Norsonic	Nor 1251	34128
Outdoor Microphones	Gras	GRA-41AL	04
UPS power supplies	Campbell	CA-1317	-
Weather Station	ClimeMET	3000	-

Table 4.2: Equipment Used

4.7 The equipment was calibrated with the same acoustic calibrator to the manufacturer's recommended levels at the beginning and end of the measurement periods and no significant drift in calibration was noted and has been detailed in the appendices of this report.

4.8 Calibration certificates have not been included but are available upon request.

5.0 NOISE MONITORING RESULTS

5.1 Whilst conducting the environmental noise survey professional judgement was used to identify the principal sources of noise across the entire site, these have been assessed to be:

- Traffic noises from vehicles travelling along the surrounding road network;
- Agricultural vehicles and operations in the area; &
- Occasional sounds such as wildlife and wind in the trees.

5.2 The following table and charts overleaf show the overall $L_{Aeq,T}$, L_{A10} , $L_{A90,T}$ and highest recorded L_{AFMax} sound levels at the monitoring location (N.B. sound levels are exclusive of periods of inclement weather):

Date	Period	T	dB $L_{Aeq,T}$	dB $L_{A10,T}$	dB $L_{A90,T}$	dB L_{AFMax}
26/07/2021	Day	8hr	36.4	38.6	24.6	63.5
	Night	8hr	35.7	37.8	16.5	62
27/07/2021	Day	15hr	38.7	40.8	27.8	68.8
	Night	7hr	33.7	36.6	16.5	62.3
28/07/2021	Day	11hr	42	44.1	33.2	67.3
	Night	8hr	35.3	38	22.7	69
29/07/2021	Day	15.5hr	40.8	43.4	33.1	76.9
	Night	5.5hr	30.7	34.8	16.1	53.2
30/07/2021	Day	10.25hr	46.3	49.6	35.6	71.9
	Night	7.5hr	37.3	39.3	30.4	62.3
31/07/2021	Day	14.5hr	41.6	40.1	27.1	67.5
	Night	8hr	33.2	34.9	17.4	64.1
01/08/2021	Day	15hr	35.9	38.5	24.5	63.9
	Night	8hr	32.8	35.9	19	62.8
02/08/2021	Day	16hr	36.8	38.1	26.4	73.9
	Night	8hr	33.5	37.6	19.8	62.7
03/08/2021	Day	16hr	36.6	38.9	28.8	61.6
	Night	8hr	34.7	36.8	23	61.3
04/08/2021	Day	3hr	39.3	41.8	32.5	62.8

Table 5.1: Noise Monitor Results

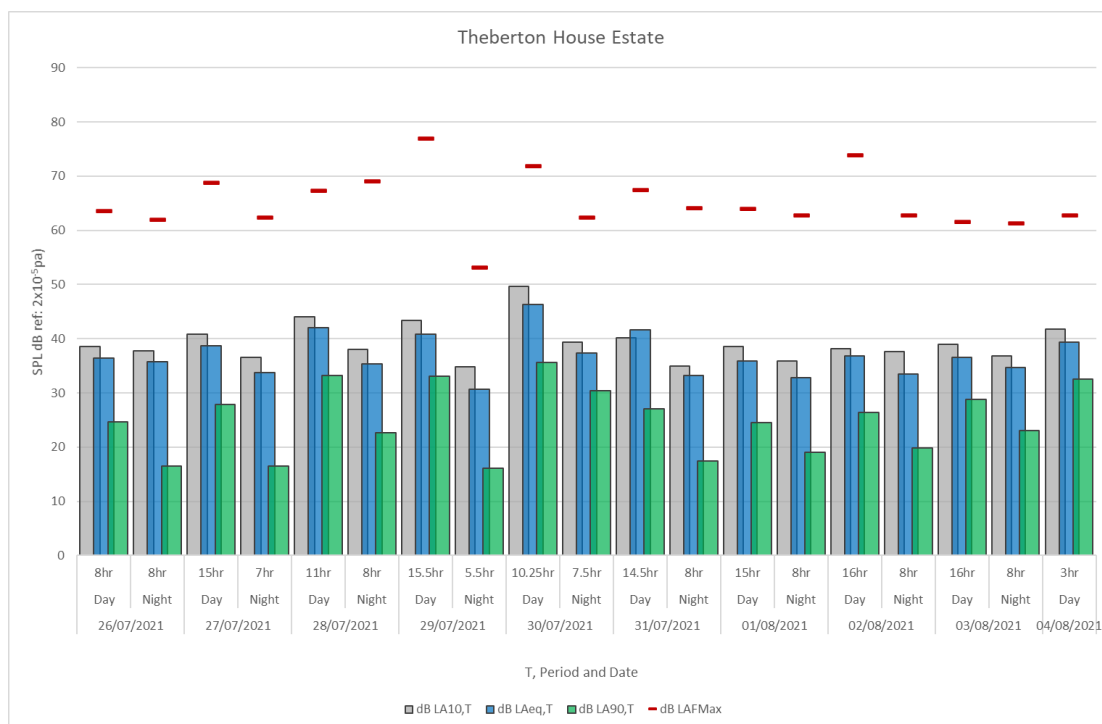


Chart 5.1: Noise Monitor Results

- 5.3 As can be seen in the table and chart above, the ambient levels remained very low, which is expected for this largely rural location. The most commonly occurring daytime ambient sound level at this location was 37 dB $L_{Aeq,1hr}$ and the daytime background sound level ranged between 18 and 39 dB $L_{A90,Day\ Time}$. The night time background sound levels were far lower, between 16 and 30 dB $L_{A90,Night(8\ hours)}$, but with a most commonly occurring night time background sound level of 30 dB $L_{A90,1hr}$.

Comparison with EDF ES Levels

- 5.4 The most representative monitor location in the EDF ES for the Theberton House Estate NSR was SLR 9, which was stated to be a typical measured daytime level of 43-44 dB $L_{Aeq,T}$. (Table 4.13, Book 6, Volume 6, Chapter 4). A detailed analysis of the measured sound levels was included within Book 6, ES Volume 2, Chapter 11, the Noise and Vibration Baseline Report.
- 5.5 Within the submitted document, the baseline sound levels were approximately 6-7 dB higher than those measured within the Create baseline sound monitoring for the day time ambient sound level, and the background sound levels were significantly higher.
- 5.6 Presumably the considerable difference was due to the reliance on three individual thirty minute measurements during the day and a single one hundred minute measurement at night time.



6.0 CONSTRUCTION NOISE - SLR

Construction Activities - Overview

- 6.1 The EDF ES provides provisional information pertaining to the 'construction sequence', which details the anticipated construction activities throughout the development, as well as some preliminary phasing and a broad stroke construction noise assessment (as discussed later within this Chapter).

Working Hours, Project Duration and Approach

- 6.2 Construction work would take place during Monday to Saturday 07:00 to 19:00 hours, with no working on Sundays or bank holidays. However, some activities may require 24-hour working and these would be notified to East Suffolk Council (ESC) in advance.
- 6.3 As the NSR location falls within the East Suffolk district, the working hours would be required to be agreed by the local authority. In accordance with East Suffolk Council, the standard working hours for construction projects is between 07:30 – 18:00 Monday to Friday and 08:00 to 13:00 on Saturdays and no working on Sundays or Bank Holidays. Whilst this time difference is minor, it is unclear whether this has been reconciled with the local authority.

EDF Construction Noise Calculations

- 6.4 The EDF ES has been divided into two phases comprising preparatory works and main phase construction work. Each phase would contain the following activities:
- Preparatory works: site set up and clearance, including trees and hedgerows, the erection of temporary fencing on land required for construction and the creation of alternative access arrangements and rights of way, setting up of the temporary contractor compounds including security, welfare facilities, and temporary utilities; and
 - Construction Works: earthworks, road construction and surfacing, construction of bridges and civil structures (including piling), utility and drainage installation, construction of pavements, kerbs, footways and paved areas, installation of permanent fencing, road signs and marking, and road lighting, permanent connections to existing road networks, and landscaping.
- 6.5 Over the specified 24-month duration, it has been stated that the Theberton House Estate receptor would experience each stage.
- 6.6 The following tables show a repeated example of the calculation methodology used. It has been assumed the sound power (L_{WA}) levels have been taken from the empirical evidence in BS5228-1:2009, which is a common practice and suitable for this application.

- 6.7 The EDF ES also recognises and states that predictions pertaining to construction related activities are broad:

“The construction arrangements described in this section provide the basis for the assessment presented in this volume. Details of construction are necessarily broad and may be subject to modification during the detailed design stage and / or once a contractor has been appointed. The construction proposals are therefore indicative only but are sufficient to enable robust assessment of a realistic ‘worst case’ assessment of likely significant effects.” – Section 2.4.2

- 6.8 As the construction noise assessment at this stage was stated to be necessarily broad, the calculations used in the EDF ES have considered the highest-level contributor for each stage only. Whereas this would be considered appropriate for an indicative assessment at the outline stages, it would not be considered a robust assessment, which should assess for the cumulative impact from all processes. An example has been shown in the following tables.
- 6.9 The table below is an excerpt from the EDF ES, which shows an example calculation method for the ‘Preparatory Works’ phase, which most closely correlates with the ‘Site set up and Clearance’ section in Table 1.1 - Volume 6 Sizewell Link Road Chapter 4 Noise and Vibration Appendices 4A - 4B. The following nomenclature applies:

r = Radial distance

A_r = Attenuation over distance

A_g = Ground attenuation

A_{met} = Meteorological attenuation

A_a = Air attenuation

A_b = Barrier attenuation

Receptor 18 Theberton House	Vegetation Clearance	TCC Pretty Road	TCC Pretty Road
Operations	Saw/chip	Centre	Edge
Source Value: $L_{Aeq,T}$ @ 40m (dB)	70/74	74	70
r , typical, m	250m	1200m	1200m
A_r	16	30	30
$A_g + A_a + A_{met}$ or $A_b + A_a + A_{met}$	3	9	9
$L_{Aeq,T}$ (dB)	51/55	35	31

Table 6.1: Equipment List

Receptor 18 Table 1.4 - Volume 6 Sizewell Link Road Chapter 4 Noise and Vibration Appendices 4A - 4B

- 6.10 The following table shows the calculations repeated (where L_{WA} has been converted into L_{PA} at 10mtrs), inclusive of all equipment items in the works phase at the 250m radial distance.

Activity	BS5228 ref	Level	% on Time	On Time Correction (dB)	Distance to Receiver (m)	Distance Correction (dB)	SPL at Receiver (dB)
Lorry loader crane HIAB	-	76	25	6	250	28	42
Diesel / petrol generators	-	69	100	0	250	28	41
360 Wheeled / tracked excavators	-	79	70	1.5	250	28	50
180 Backhoe loaders	-	79	50	3	250	28	48
Dump Trucks	-	78	70	1.5	250	28	49
Telehandlers	-	79	50	3	250	28	48
Chainsaws and brush-cutters	-	87	17	9	250	28	50
Wood chippers	-	93	17	9	250	28	56
Road sweeper / gully sucker	-	79	50	3	250	28	48
Vibratory tamping rollers	-	83	50	3	250	28	52
- (Ag + Aa + Amet or Ab + Aa + Amet)							3
Resultant SPL (dB) at Receiver:							57

Table 6.2: Repeated Calculations

- 6.11 Whilst agreed as an appropriate indicative approach, the predicted increase of 6 dB over the EDF ES levels emphasizes the inherent uncertainty associated with relying on these provisional calculations alone, as there remains the possibility that these operations can occur simultaneously or 'overlap' with one another. The impact of a construction project should be assessed over a complete hour or daytime period, hence the reliance on the percentage on time function. This highlights the necessity for further, site specific assessments once method statements have been submitted, and inclusion of the findings into the CMP.
- 6.12 We have calculated the construction activities for the individual elements as defined in the Construction Assumptions within Book 6, Volume 6, Chapter 4, Appendix 4B, which have been included within Table 6.3 below. As stated in the ES, it has been expected that Theberton House Estate would experience all phases throughout construction, the minimum distance of 250mtrs has been used to assess the impact from each phase at this distance. This has been compared to the representative daytime ambient level as defined in Section 5.3 of this report:

Works Phase	Activity	SPL at NSR (dB)	Cumulative SPL at NSR for Phase (dB)	Averaged Daytime SPL at NSR
Preparatory	Site set up and Clearance	57	57	40 dB L _{Aeq,T}
Construction	Earthworks	55	64	
	Drainage	54		
	Pavements	58		
	Kerbs, Footways and Paved Areas	57		
	Bridges and Civil Structures	57		
	Road Restraints	51		
	Fencing	51		
	Traffic Signs	49		
Road Lighting	48			

Table 6.3: Construction Noise Calculations

- 6.13 As can be seen in the table above, all activities are predicted to be in excess of the residual ambient level at this location. The cumulative effect of Construction Phase would be 24 dB above the residual ambient level. As mentioned previously, there would be the potential for construction activities to run concurrently with one another, so there would be the potential

for source summing at the NSR. For example, the level sum of 'Pavements' and 'Kerbs, Footways and Paved Areas' would result in a ≈ 61 dB level at the NSR.

- 6.14 In Table 4.9 of Book 6, Volume 6, Chapter 4, the EDF ES also goes on to define the usage of LOAEL and SOAEL values in the assessment. The descriptions and associated actions were reported to have been discussed with local authorities between 2015 and 2019. The NPSE, NPS and PPG require the assessment of noise (and vibration) against the Lowest Observed Adverse Effect Level (LOAEL) and the Significant Observed Adverse Effect Level (SOAEL).
- 6.15 Definition of each is dependent on certain variables including residual levels, duration, frequency of occurrence and general context. In instances such as this, there is guidance for determining these effects, for which the EDF ES has correctly identified the Design Manual for Roads and Bridges LA 111 Noise and Vibration Document (May 2020), in which the document defines the LOAEL as the baseline dB $L_{Aeq,T}$ levels, and the SOAEL is determined from the values in Table E.1 of BS5228-1 (Table 3.12 LA 111), which pertains to the ABC method category thresholds, for which this NSR, would be defined as Category A (65 dB $L_{Aeq,T}$).
- 6.16 In section Book 6, Volume 6, 4.3.36 of the EDF ES however, the values within Table E.2 of BS5228-1 have been used to define the LOAEL/SOAEL, which if assessed against the 08:00 – 18:00 relevant time period, would be 75 dB (10 dB greater than the Category A threshold). The reason for this is explained within section Book 6, Volume 6, 4.3.31-32:

“The NPSE, the NPSs and the PPG require the assessment of noise and vibration against the lowest observed adverse effect levels (LOAEL) and the significant observed adverse effect levels (SOAEL). These will differ on variables such as the level and character of the noise or vibration source, timings of when it would occur, its duration, existing sounds present and the frequency of the occurrence of the source.

Each different source type requires its own specific value for LOAEL and SOAEL, which depends on these factors. The methodology for assigning significance differs from the general methodology set out in Volume 1 Chapter 6 of the ES, as it does not allow for these variables to be properly considered. Each source has therefore been considered separately and values for LOAEL and SOAEL defined for different sensitivities.”

- 6.17 The NPSE was published in March 2010 and the ProPG: Planning and Noise was issued in May of 2017. The ProPG document relates to new residential development and is therefore not considered relevant in this application. Although we agree that this approach is suitable in some applications, we believe that the most recent DMRB methodology should be used. Therefore, the LOAEL should be defined by the existing ambient sound level and the SOAEL should be defined by the Category A Threshold within BS5228-1. The previously described Negligible Impact would therefore require reclassification.

- 6.18 The following table is an excerpt from Table 4.16 of the ES: *Summary of predicted construction noise effects at the nearest noise sensitive receptor locations around the site at different periods* in which the significance of effects has been determined:

Receptor		Mon-Fri 07:00 to 19:00 Hours and Sat 07:00 to 13:00 Hours		Saturday 13:00 to 19:00 Hours	
		Preparatory Works	Main Construction Phase	Preparatory Works	Main Construction Phase
18	Theberton House	Negligible	Moderate adverse, significant	Minor adverse, not significant	Major adverse, significant

Table 6.4: EDF ES Significance of Effects

- 6.19 We agree that the impact of the Main Construction Phase would be classed as significant irrespective of the classification and warrants mitigation.

In Summary

- 6.20 The results and predictions presented in the EDF ES would be considered suitable for the ES stage in the development. The 6 dB discrepancy in the resultant sound levels would be regarded as marginal, given the basis of assessment has been professional judgement alone as opposed to project and site-specific method statements. We strongly urge that a more detailed and exhaustive construction noise and vibration assessments should be undertaken once works processes have been finalised. This would inform the assessment of secondary mitigation measures.
- 6.21 Whereas the calculable level of 51/55 dB (57 dB by Create's cumulative assessment) would not be defined as being above the SOAEL (in accordance with LA 111), it is a considerable increase above the existing measured daytime ambient sound level of 37 dB $L_{Aeq,1hr}$ at the Theberton House location.
- 6.22 This level, subsequently the magnitude of change, is representative of the level at 1mtr from the residence's façade and does not consider the level in any external amenity spaces within the property boundary. As can be seen in Figure 4.1, the grounds of Theberton House Estate extend to the boundary of the proposed route of the SLR and would therefore be exposed to greater sound levels than at the residence.
- 6.23 The noisiest activity, paving, would result in sound levels in the region of 72 dB $L_{Aeq,1h}$ at a distance of 50m from the road. These sound levels would typically increase the closer to the road, should the residents choose to use their entire grounds.
- 6.24 A level of annoyance for external amenity spaces is stated in WHO community noise guidelines and has been reflected in the BS8233:2014 guidance for external amenity spaces. Typical

design targets for new dwellings are 50 dB $L_{Aeq,T}$, but do not apply to sounds with definable characteristics (this is commonly exclusive of most sources except for traffic noise). As the residence is pre-existing, it would not be regarded as appropriate to assess any resultant impact against these targets, but should prove to be a useful indicator for any potential loss of amenity. It must be noted that the measured sound level show that the external amenity spaces currently fall within these levels.

7.0 CONSTRUCTION NOISE - MAIN DEVELOPMENT ROUNDABOUT

7.1 The Theberton House Estate lies towards the West of the existing Sizewell Power Station and as part of the access arrangements to serve the proposed scheme, a new five-arm roundabout is proposed on the B1172 Abbey Road to the East of Leiston Abbey. This is approximately 700mtrs from the NSR's residence and approximately 200mtrs from their amenity space.

7.2 As this was part of the Main Development site, it was not considered as part of the SLR submission. Evaluation of the main development documentation appears to show that this was not 'screened in' as part of the assessment. Review of the Yoxford roundabout documentation provides some rationale which may be applicable to why this site was not assessed. The following has been quoted from the Yoxford Roundabout documentation in section 4.3.12, Book 6, Volume 7, Chapter 4:

"All receptors within 300 metres (m) of the proposed development (for the highway improvement works screened in to the assessment) have been considered, where there is a potential for the level of construction noise or vibration to exceed a negligible effect."

7.3 Should this be the reason, then the new Main Development Roundabout would have been 'screened out', given the distance. This screening however only includes NSR dwellings and does not include amenity spaces, which in the case of Theberton House Estate, would be significantly impacted as it approximately 200mtrs from the proposed roundabout.

7.4 The following tables show the ES stated works phases (both singularly and cumulatively) at the NSR dwelling distance of 700mtrs and external amenity minimum distance of 200mtrs:

Levels at Approximated 700mtr Distance from Roundabout to NSR Dwelling				
Works Phase	Activity	SPL at NSR (dB)	Cumulative SPL at NSR for Phase (dB)	Averaged Daytime SPL at NSR
Preparatory	Site set up and Clearance	45	45	40 dB L _{Aeq,T}
Construction	Earthworks	44	52	
	Drainage	42		
	Pavements	46		
	Kerbs, Footways and Paved Areas	45		
	Bridges and Civil Structures	45		
	Road Restraints	39		
	Fencing	39		
	Traffic Signs	37		
	Road Lighting	36		

Table 7.1: Level at NSR Dwelling - 700mtrs (- A_g + A_a + A_{met} or A_b + A_a + A_{met} = 6 dB)

Levels at Approximated 200mtr Distance from Roundabout to NSR External Amenity				
Works Phase	Activity	SPL at NSR (dB)	Cumulative SPL at NSR for Phase (dB)	Averaged Daytime SPL at NSR
Preparatory	Site set up and Clearance	60	60	40 dB L _{Aeq,T}
Construction	Earthworks	58	67	
	Drainage	57		
	Pavements	61		
	Kerbs, Footways and Paved Areas	59		
	Bridges and Civil Structures	60		
	Road Restraints	54		
	Fencing	54		
	Traffic Signs	52		
	Road Lighting	51		

Table 7.2: Level at NSR External Amenity - 200mtrs (- $A_g + A_a + A_{met}$ or $A_b + A_a + A_{met} = 2$ dB)

- 7.5 The above tables show that most the works processes would be audible at the dwelling distance, whereas the level at the external amenity would be most significantly impacted. All works processes for the external amenity area have been predicted to exceed the residual ambient and are indicative of a significant adverse impact which would warrant mitigation.

8.0 CONSTRUCTION NOISE – C5, C6 & C7.

8.1 Guidance to the prediction and assessment of the construction phase noise effects has been taken from BS5228-1:2009+A1:2014, which provides recommendations for basic methods of noise control relating to construction and open sites where work activities and operations could potentially generate significant noise levels.

BS5228-1 – Noise

8.2 The annexes to BS5228-1 provide information on the following:

- Relevant legislation – Annex A;
- Typical noise sources and advice on methods for mitigating the noise from these sources – Annex B;
- Sound level data for various phases – Table C.1 has been heavily referenced in this assessment as it relates to plant and equipment used for typical demolition activities;
- Methods of how to assess the significance of these noise effects including the ABC method and the 2-5dB(A) Change methods – Annex E;
- Methods for estimating the noise from these activities on sites, including adjustments for distance, percentage on time etc – Annex F; and
- Suggestions or noise monitoring – Annex G.

8.3 Other specific noise sources and considerations are also included but not relevant in this instance, for example, noise from piling, over pressure from materials falling from heights and blasting works.

BS5228-1:2009+A1:2014: “The ABC Method”

8.4 The ‘ABC Method’ as outlined in section E.3.2 of BS5228-1:2009+A1:2014 defines threshold values for permissible levels of noise generated by site operations. In essence, the residual ambient noise level ($L_{Aeq,T}$) is determined and rounded to the nearest 5 dB. This is then compared with the site generated noise and if the noise level exceeds the appropriate category value, then a potential significant effect is indicated.

Assessment category and threshold value period	Threshold value, in decibels ($L_{Aeq,T}$) (dB)		
	Category A	Category B	Category C
Daytime (07:00 – 19:00)	65	70	75

Table 8.1: ABC Method. (dB ref: 2×10^{-5} pa): [Excerpt from BS5228-1:2009+A1:2014, Table E.1 p:125]

- 8.5 In this instance, the most commonly occurring ambient sound level was measured to be ≈ 37 dB(A) $L_{Aeq,1hr}$ at Theberton House Estate (which has been deemed as representative) so the 65 dB(A) threshold (Category A) has been used in this assessment.

Construction Activities - Overview

- 8.6 As previously stated, the proposed construction timings have been comprised of 5 distinct phases (with anticipated, inevitable overlap). Given the nature of the works and the locality of the NSR, the works in Phase 1 pose the greatest risk.

Working Hours

- 8.7 Section 3.3.12 and Table 3-1 of Book 6.3, Volume 2, Chapter 3 – Description of Construction outlines the anticipated working patterns, although it is unclear what times pertain to the zones in question:

“The majority of workers are expected to be working on either an early shift or a late shift. Most of the remaining employees would work to office hours.” – Section 3.3.12

Shift	Start Time	End Time
Early Shift	06:00–08:30	14:00–18:30
Late Shift	13:30–15:00	22:00–00:00
Night Shift	20:30–22:00	06:00–08:00
Office Shift	07:30–09:00	17:30–19:00

Table 8.2: Construction Shift Patterns Table 3-1 Book 6.3, Volume 2, Chapter 3

- 8.8 As the NSR location falls within the East Suffolk district, the working hours would be required to be agreed by the local authority. In accordance with East Suffolk Council, the standard working hours for construction projects is between 07:30 – 18:00 Monday to Friday and 08:00 to 13:00 on Saturdays and no working on Sundays or Bank Holidays. Whilst this time difference is minor, it is unclear whether this has been reconciled with the local authority.
- 8.9 The ES chapter goes on to state activities which would generally be undertaken during the night shift, which includes ‘removal of excavated material’, although this has been assumed to be at the coastline.

EDF Construction Noise Calculations

- 8.10 The Temporary Construction Area (TCA) refers to the main area of land that would be required largely on a temporary basis to facilitate the construction of the proposed development. This land would primarily be located to the north of the Sizewell Marshes SSSI between the B1122 and the coast, to the north-west of the main platform, and is the closest area of the site to the NSR.

8.11 The table below shows calculation of the stated equipment to be used (as defined in Annex 11B/B of Book 6, Volume 2, Chapter 11). It has been assumed the sound levels presented in the ES have been taken from the empirical evidence in BS5228-1:2009+A1:2014, which is a common practice and suitable for this application.

8.12 These noise levels have been corrected for relevant attenuation (distance, ground, barrier, air, meteorological where applicable) but do not include any other aspects of mitigation, including site hoarding, bunding etc.

8.13 In Book 6, Volume 2, Chapter 11, the EDF ES also recognises and states that predictions pertaining to construction related activities at this stage are not based on method statements or confirmed works processes:


“Chapter 3 of this volume sets out the assumed indicative approach to construction. This represents the most likely approach to construction given the site constraints and Sizewell C project requirements. The proposals do enable a robust assessment of the likely effects, although the absence of final, confirmed construction details creates some challenges for noise prediction.” – Section 1.3.1.2

8.14 Whereas this would be considered appropriate for an indicative assessment at the outline stages, we disagree that it would be regarded as a robust assessment. A robust assessment would include assessment from confirmed method statements and be inclusive of cumulative effects from all works stages. An example of indicative calculations for the stated phases, equipment, quantities and percentage-on-times has been shown in the following table:

Works Area	Distances (m)	Activity	SPL at NSR	Cumulative SPL at NSR for Phase	Averaged Daytime SPL at NSR
SITE	600	Phase 1-1a 'Felling'	53	59	40 dB L _{Aeq,T}
SITE	600	Phase 1-1b 'Stripping/Levelling'	58		
SITE	600	Phase 1-1c 'Water Management Zone'	39		

Table 8.3: Construction Noise at Theberton House (No Mitigation)

8.15 The table above shows that without mitigation, Phase 1 would not be predicted to exceed the Category A threshold as defined in BS5228-1 (as described in section 7.4 of this report). Whereas assessment against this criterion has shown all activities to be below this threshold, it does not factor the considerable loss of amenity that would be experienced at the NSR, for which the residual ambient would be exceeded in all instances. Given the proposed works duration for these phases of 4 years (section 2.3 of this report), this equates to a considerable degree of change in ambient levels.

8.16 Book 6, Volume 2, Chapter, Appendices 11B includes the 3D noise propagation model used to determine the effects at the NSR. The following images can be found in the aforementioned document on pages 203 – 206. Note the residual ambient measured at the location (40 dB) is below the lowest contour in the legends ( <= 42).

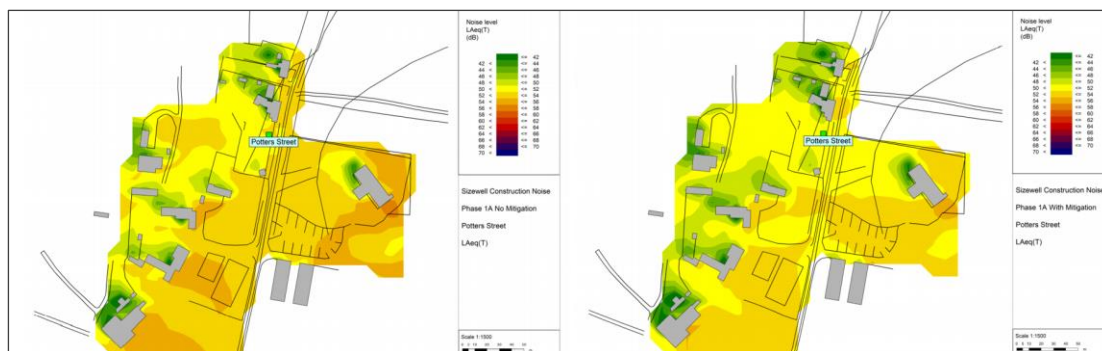


Figure 8.1: Phase 1a: No Mitigation Left & Phase 1a: With Mitigation Right

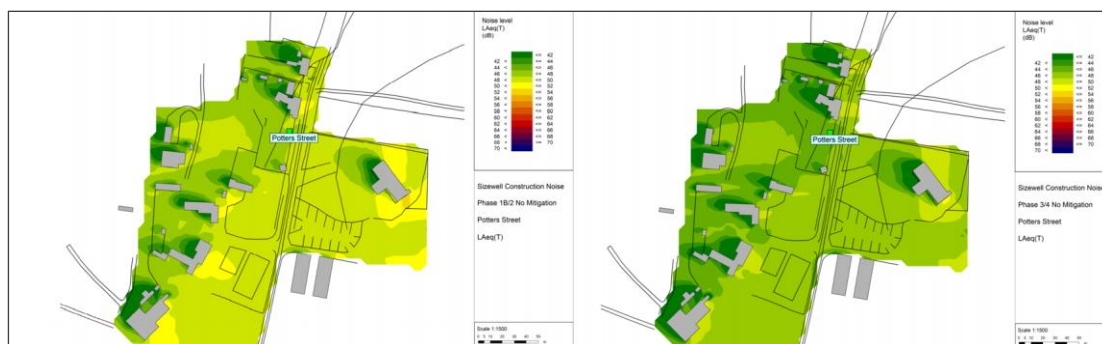


Figure 8.2: Phase 1b/2: No Mitigation Left & Phase 1b/2: With Mitigation Right

- 8.17 It can be seen in the figures above that in all instances (both with and without mitigation), the predicted ambient would exceed the residual ambient measured. Given the works duration of >4 years, this change would be regarded as noticeable and detrimental.
- 8.18 Table 11.32 in Book 6, Volume 2, Chapter 11 defines the residual effects following mitigation at the various receptors around the site, for which receptor 18 is Theberton House Estate. The following table shows the assessment of effects following primary, tertiary, and additional mitigation measures during the works phases 1a and 1b:

Receptor	Impact	Primary or Tertiary Mitigation	Assessment of Effects	Additional Mitigation	Residual Effects
Theberton House (18)	Phase 1a	Embedded landscape bunds and/or acoustic screens as described in section 11.5 and listed in Appendix 11B	Minor Adverse	Secondary acoustic screens as described in section 11.7 and Appendix 11B.	Minor Adverse (Not Significant)
	Phase 1b/2	Best practice measures set out within the CoCP (Doc Ref 8.11).		Noise mitigation scheme to be applied as appropriate.	Minor Adverse (Not Significant)

Table 8.4: Summary of Effects for Construction Phase

- 8.19 This assessment does not consider the amenity space for Theberton House, which is considerably closer and would experience far greater noise levels.

In Summary

- 8.20 The results and predictions presented in the EDF ES would be considered suitable for the ES stage in the development, however we strongly urge that a more detailed and exhaustive construction noise and vibration assessments should be undertaken once works processes have been finalised. This should include assessment of the efficacy of all additional mitigation measures.
- 8.21 This level, subsequently the magnitude of change, is representative of the level at 1mtr from the residence's façade and does not consider the level in any external amenity spaces within the property boundary. As can be seen in Figure 4.1, the grounds of Theberton House extend further south towards the main development site and would therefore be exposed to far greater sound levels than at the residence. Any stated sound levels therefore, would typically increase the closer to the Main Development Site, should the residents choose to use their entire grounds.
- 8.22 A level of annoyance for external amenity spaces is stated in WHO community noise guidelines and has been reflected in the BS8233:2014 guidance for external amenity spaces. Typical design targets for new dwellings are 50 dB $L_{Aeq,T}$, but do not apply to sounds with definable characteristics (this is commonly exclusive of most sources except for traffic noise). As the residence is pre-existing, it would not be regarded as appropriate to assess any resultant impact against these targets, but should prove to be a useful indicator for any potential loss of amenity. It must be noted that the measured sound level show that the external amenity spaces currently falls below this threshold.

9.0 TRAFFIC AND TRANSPORT

- 9.1 A total of 14 measurement locations have been identified in the noise and vibration chapter (6.7 Volume 6 Chapter 4) of the ES. The survey locations used in the assessment of the new road have been identified as positions RT2, RT3, RT4, RT6, RT15, SLR1, SLR2, SLR3, SLR4, SLR5, SLR6, SLR7, SLR8 and SLR9.
- 9.2 The EDF ES states that the 'study area' includes all noise and vibration sensitive receptors within 300 metres of the new road for construction works and within 600 metres of the new road or other affected roads for operational noise levels, in accordance with recommendations in DMRB, LA111. As the Theberton House estate lies within both of these distances, assessment was warranted.
- 9.3 The assessment of road traffic noise in the EDF ES have been undertaken for two distinct scenarios:

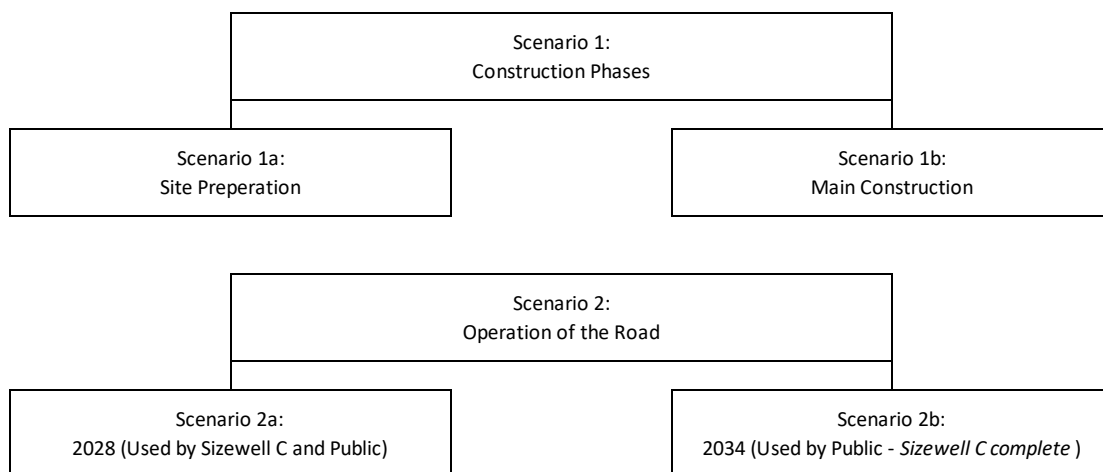


Figure 9.1: Traffic and Transport Assessment Scenarios

- 9.4 The noise and vibration chapter (6.7 Volume 6 Chapter 4) stated that in order to assess noise from the future link road a computer model was constructed, which used traffic flow count predictions for the following scenarios:
- 2023 early years;
 - 2028 peak construction 'typical day';
 - 2028 peak construction 'busiest day'; and
 - 2034 operational traffic.
- 9.5 Each scenario has been compared against the equivalent period with traffic flow predictions adjusted for natural growth, as though the development did not go ahead.
- 9.6 It was unclear from the reports how (or if) the survey measurements were used to validate the propagation characteristics of the computer model. This is not strictly a requirement but

is considered to be good practice to calibrate the noise model. It was stated in paragraph 4.4.6 of the noise and vibration chapter (6.7 Volume 6 Chapter 4) that:

“The baseline noise levels used for the assessment of road traffic noise are those predicted by modelling. Measured levels do not always match modelled values as measurements were generally made close to receptors in publicly accessible locations rather than at the receptor itself, and measurements are highly dependent on prevailing conditions during the survey whereas modelled values are based on annually averaged traffic data.”

- 9.7 Although we do not disagree with this statement, this is precisely why a survey may involve measurements over several days, weeks, or even a full year to allow for short term variations in noise climate to be accounted for.
- 9.8 In some cases, the Sharps Redmore report site measurements were found to be in excess of 10 dB above their predicted levels, once the 2 dB reduction was accounted for when converting between $L_{10,18\text{-hour}}$ and $L_{Aeq, 16\text{-hour}}$ in accordance with BS8233:2014 and the TRL document for converting the UK road traffic noise index $L_{A10,18h}$ to the EU noise indices for road mapping. Through review of the survey notes it would appear that this anomaly was mainly due to local wildlife dominating the noise environment. Considering that only 30 minute measurements were used, it is confusing why this location was used, if there was continuous additional noise witnessed.
- 9.9 The acoustic climate at this location was reported to consist of birdsong, road traffic noise, occasional aircraft and at times a diesel water pump in a nearby field. The water pump emitted a low level, continuous sound which contributed to the background sound level. The afternoon survey was undertaken over two days and the pump remained operable. There was no details of the weather at the time of the monitoring, although the statement about the diesel pump being less detectable with a different wind direction does add further uncertainty.
- 9.10 We have reviewed some of the hourly traffic flow data contained in the appendix (6.7 Volume 6 Chapter 4 Appendix 4A - 4B) with the hourly counts contained in the transport assessment (6.3 Volume 2 Chapter 10) and found that the data correlated well (within 2%). The reason for any discrepancies was not clear and not discussed in the report, but in practice small changes in traffic flows will not significantly alter the outcome of their report.
- 9.11 We have attended the site and carried out our own measurements as shown in Appendix B. Our long-term measurements were within 3 dB from the results of the Sharps Redmore computer model, and we therefore would expect their proposed methodology to be suitable given the information available.

In Summary

- 9.12 We believe the results of the Sharps Redmore predictions are likely to be reliable, given the information currently available.
- 9.13 The Sharps Redmore report stated that this site will be subject to the following changes in noise levels:

Period	Daytime $L_{A10, 18\text{-hour}}$	Night-time L_{night}
Baseline 2028	46.4 dB	37.2 dB
Typical day 2028	50.3 dB	43.7 dB
Difference (Effect)	3.9 dB (Moderate adverse)	6.5 dB (Major adverse)
Peak day 2028	50.8 dB	43.8 dB
Difference (Effect)	4.4 dB (Moderate adverse)	6.6 dB (Major adverse)
Baseline 2034	46.6 dB	37.3 dB
Typical day 2034	47.5 dB	39.5 dB
Difference (Effect)	1.1 dB (Negligible)	2.3 dB (Negligible)

Table 9.1: Assessment of impacts

- 9.14 It can be seen that the short-term impact for the site is considered major while the long-term impact is negligible.
- 9.15 When compared to the existing measured daytime ambient sound level of 40 dB $L_{A10,18h}$ the effect is more noticeable, which would result in a difference of 7.5 dB which would be considered Major Adverse in the short term and Moderate Adverse in the long term. In line with Table 3.58 of the DMRB LA111, this is considered significant.
- 9.16 The WHO Guidelines for Community Noise indicates that moderate annoyance can occur when outdoor amenity spaces exceed 50 dB(A). Again, assuming the 2 dB reduction to convert $L_{A10, 18\text{-hour}}$ to $L_{Aeq, 16\text{-hour}}$ it can be seen that the external levels are likely to exceed this during the day. We would recommend that further mitigation measures are designed to reduce noise levels in amenity areas to below this level.

10.0 CONCLUSIONS

- 10.1 Create Consulting Engineers have undertaken a review of the Environmental Noise statement associated with the Sizewell Link Road (SLR) for the Sizewell C development plans.
- 10.2 The results from a noise survey carried out by Create have been used in support of this assessment, to compare against those presented within the EDF ES. The ES stated levels were found to be ≈ 6 to 7 dB greater than those measured by Create, although not directly comparable in terms of location.
- 10.3 Although indicative, the construction noise calculations provided by EDF should not be considered as robust or exhaustive, as they are suitable for outline scoping only. Primary measures of mitigation have been determined to be necessary within the ES, however further assessment would be warranted to determine whether secondary mitigation would be required.
- 10.4 The transport noise assessment within the ES was found to be within acceptable tolerances, and the stated significance/magnitude of effects within the ES apply. When comparing these levels to the measured sound levels however, the significance was found to increase from Not Significant to Significant.
- 10.5 The ES does not consider loss of external amenity, for which it has been assumed would be potentially significant, depending on the context as the extent of the amenity spaces. This should be considered when defining suitable measures of mitigation.
- 10.6 We are seeking a full and conclusive construction noise and vibration assessment be completed for the Sizewell Link Road and the Main Development Site once the method statements have been finalized and suitable noise mitigation be implemented to reduce the impact of the construction noise.
- 10.7 The use of earth bunds are limited at best and would be required to be positioned either close to the receptor or the noise source to maximise their efficacy. The SoundPlan model has shown that at this location, the proposed noise mitigation would only achieve approximately 2 dB reduction in sound levels. Additional near field screening would be required around some of the noisier items of plant.
- 10.8 The use of Best Practicable Means (BPM) must be adhered to, which should include the use of mufflers or silencers, nearfield screening, considerate placement of noisy plant, starting the ignitions in a synchronized manner and not leaving the engines running when not in use. These are examples only and by no means are an exhaustive list.

11.0 DISCLAIMER

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APPENDICES

APPENDIX A

Glossary of Acoustic Terminology

dB(A)

The human ear is less sensitive to low (below 125Hz) and high (above 16kHz) frequency sounds. A sound level meter can be used to duplicate the ear's variable sensitivity to sound across a spectrum of frequencies. This is achieved by building a filter into the instrument with a similar frequency response to that of the average ear. This is called an "A-weighting filter". Measurements of sound made with this filter are called A-weighted sound level measurements and the unit is dB(A).

$L_{eq,T}$

The sound from noise sources often fluctuates widely during a given period of time. An average value can be measured, the equivalent sound pressure level L_{eq} . The L_{eq} is the equivalent sound level which would deliver the same sound energy as the actual fluctuating sound measured in the same time period (T).

$L_{10,T}$

This is the minimum level exceeded for not more than 10% of the time period (T). This parameter is often used as a "not to exceed" criterion for noise.

$L_{90,T}$

This is the minimum level exceeded for not more than 90% of the time period (T). This parameter is often used as a descriptor of "background noise" for environmental impact studies.

L_{fmax}

This is the maximum sound pressure level that has been measured over a period using a fast time constant.

Octave Bands

In order to completely determine the composition of a sound it is necessary to determine the sound level at each frequency individually. Usually, values are stated in octave bands. The audible frequency region is divided into 10 such octave bands whose centre frequencies are defined in accordance with international standards.

Addition of noise from several sources

Noise from different sound sources combine, on a logarithmic scale, to produce a sound level higher than that from any individual source. Two equally intense sound sources operating together produce a sound level which is 3dB higher than one alone and 3 identical sources produce a 5dB higher sound level.

Attenuation by distance

Sound which propagates from a point source in free air attenuates by 6dB for each doubling of distance from the noise source. Sound energy from line sources (e.g. stream of cars) drops off by 3dB for each doubling of distance.

Sound Exposure Level (SEL)

This is the level at the reception point which, if maintained constant for a period of 1 second, would cause the same A weighted sound energy to be received as is actually received from a given noise event. The SEL is used to categorise and quantify the noise generated by individual railway vehicles and individual trains. As such, it serves as a “building block” to determine the L_{Aeq} for the total flow of trains over a given time period.

Subjective impression of noise

Sound intensity is not perceived directly at the ear; rather it is transferred by the complex hearing mechanism to the brain where acoustic sensations can be interpreted as loudness. This makes hearing perception highly individualised. Sensitivity to noise also depends on frequency content, time of occurrence, duration of sound and psychological factors such as emotion and expectations. The following table is a reasonable guide to help explain increases or decreases in sound levels for many acoustic scenarios.

Change in sound level (dB)	Change in perceived loudness
1	Imperceptible
3	Just barely perceptible
6	Clearly noticeable
10	About twice as loud
20	About 4 times as loud

Barriers

Outdoor barriers can be used to reduce environmental noises, such as traffic noise. The effectiveness of barriers is dependent on factors such as its distance from the noise source and the receiver, its height and its construction.

Reverberation control

When sound falls on the surfaces of a room, part of its energy is absorbed and part is reflected back into the room. The amount of reflected sound defines the reverberation of a room, a characteristic that is critical for spaces of different uses as it can affect the quality of audio signals such as speech or music. Excess reverberation in a room can be controlled by the effective use of sound-absorbing treatment on the surfaces, such as fibrous ceiling boards, curtains and carpets.

APPENDIX B

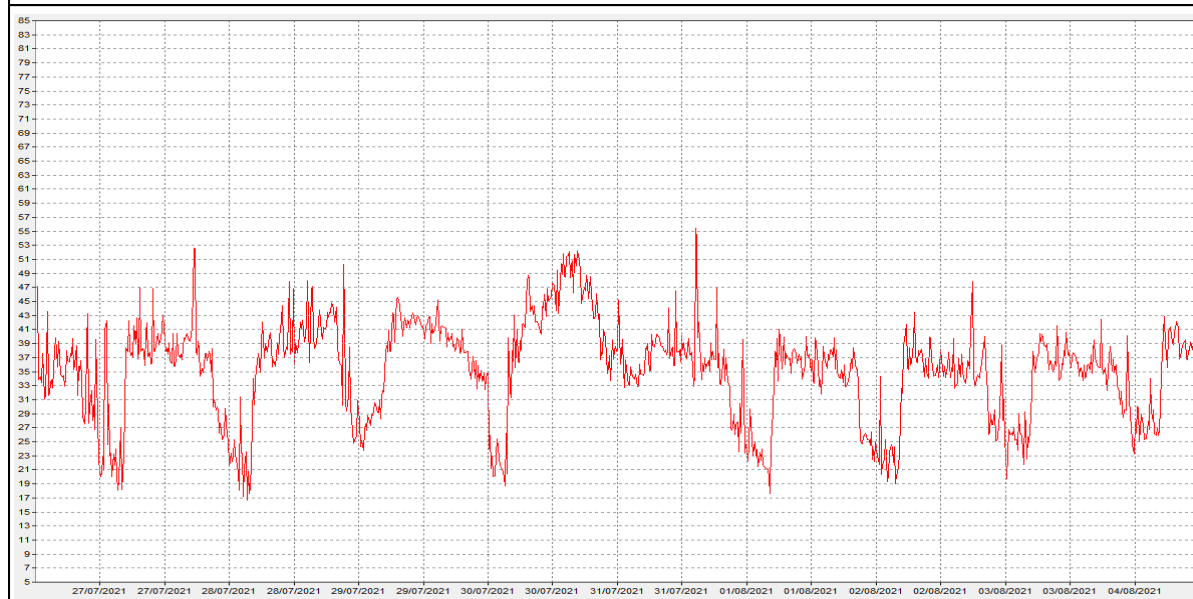
Survey Results

Project title	Theberton House Estate - Sizewell C				
Project number	P21-2319				
Date & Time of Deployment	26/07/21 - 14:00		Duration		8d 23h 20m 1s
Sound level meter and calibrator model	Nor140 RTA with GRAS 141A Outdoor Microphone & C1251 Calibrator				
Calibration ref. level	114 dB	Before	114 dB	After	114 dB
Person in charge of measurements	Sam Ward				
Other people present	n/a				
Weather station make and model	ClimeMet CM3000				

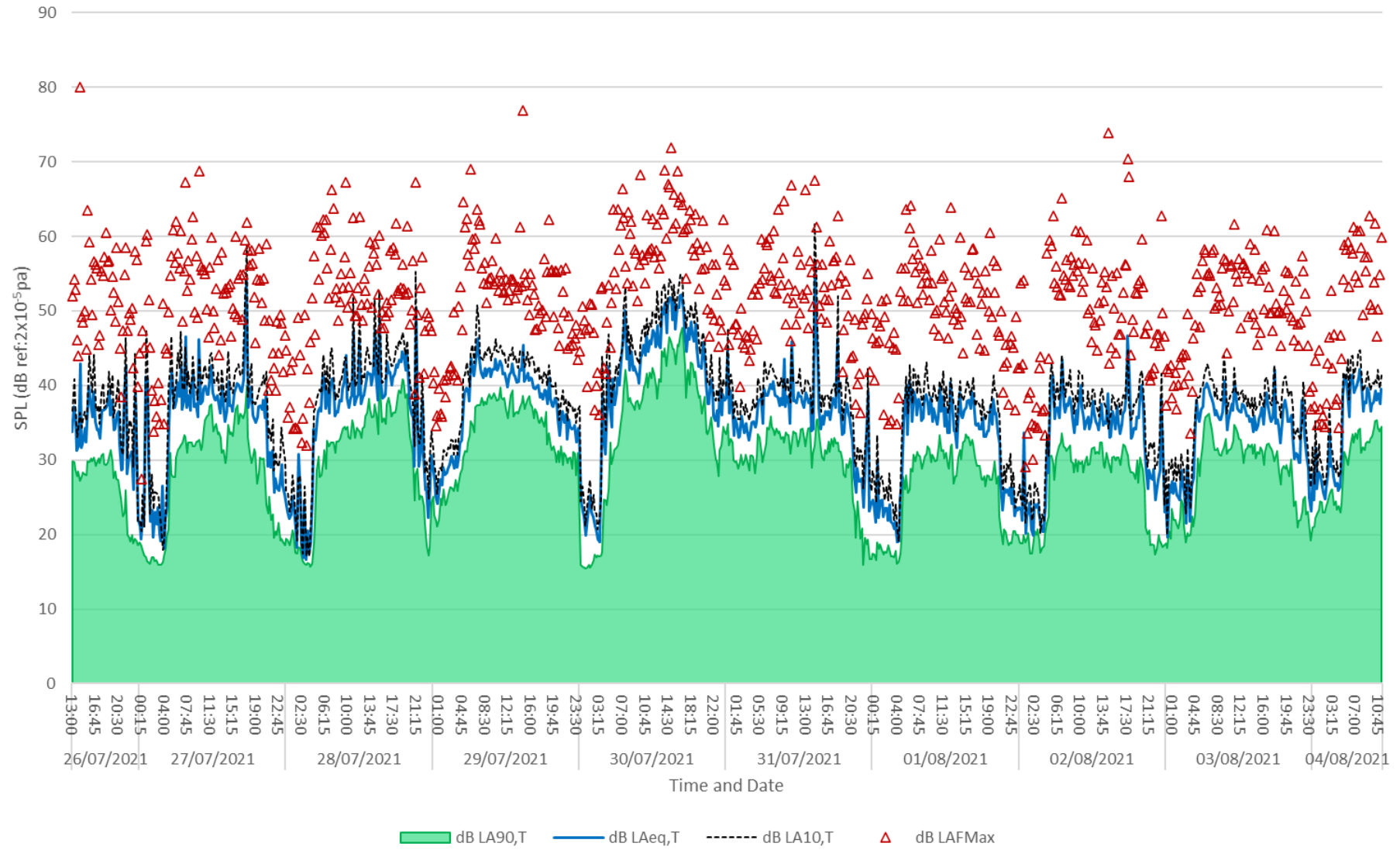
Site description:

Site was in a rural setting, surrounded by agricultural lands. High density of trees in the surrounding area, with no direct line of sight to any roads. However, the B1122 (approx 250m south) was perceptible at times. No other major roads in vicinity of the site. House is Grade I listed and as such only has single glazing throughout. Large amounts of the garden space surrounding the house used as amenable areas, with a shingle drive up to the property.

Measurement location(s)	Ref No:	Photo(s)
		



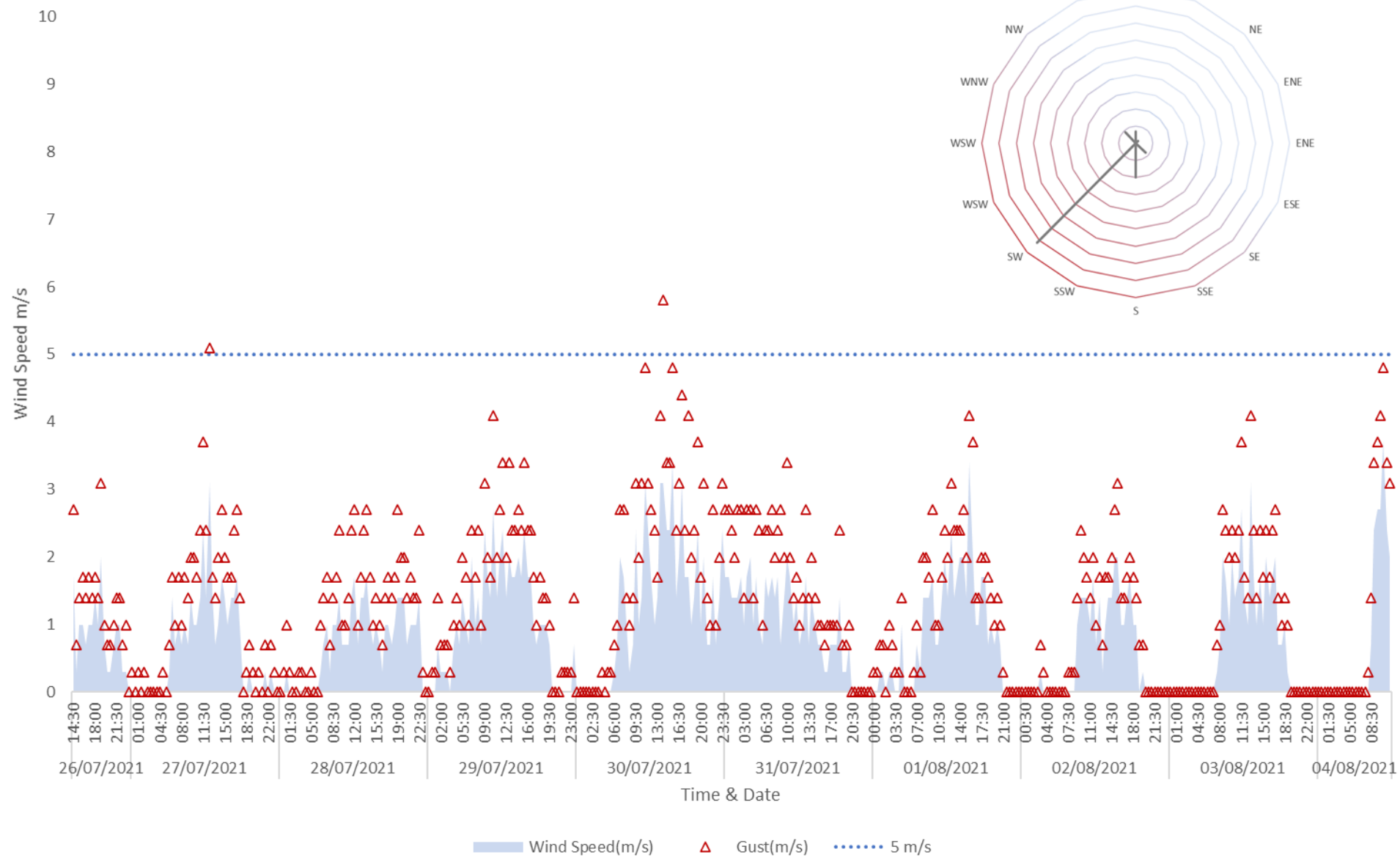
Theberton House Survey Data



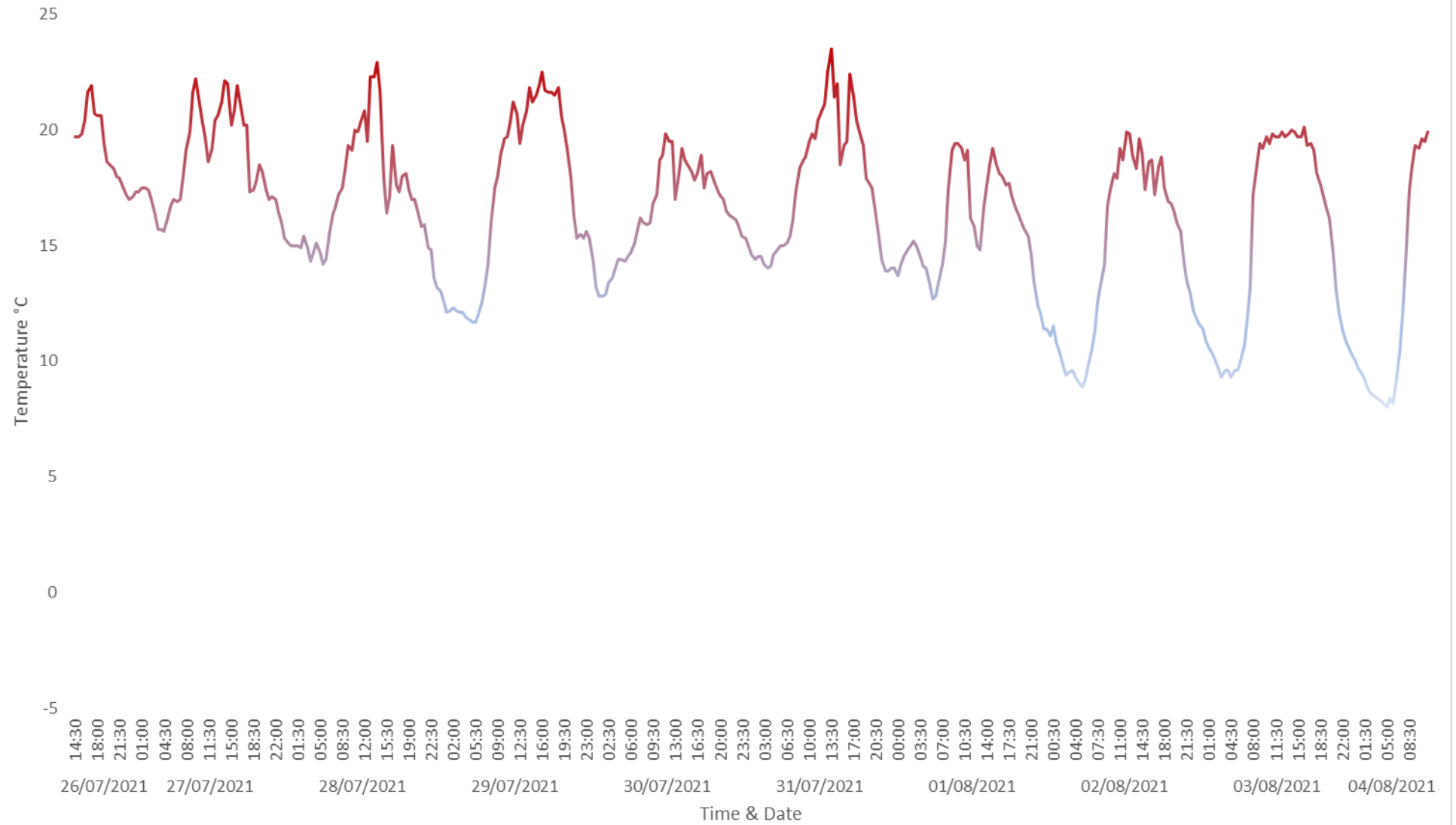
APPENDIX C

Weather Data

Wind Speed & Direction



Outdoor Temperature(°C)



Outdoor Temperature(°C)

Rainfall (mm/30min)

